



# Challenge and Solution of Characterizing Glass Transition Temperature for Conjugated Polymers by Differential Scanning Calorimetry

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**ABSTRACT:** Thermomechanical properties of polymers highly depend on their glass transition temperature ( $T_g$ ). Differential scanning calorimetry (DSC) is commonly used to measure  $T_g$  of polymers. However, many conjugated polymers (CPs), especially donor–acceptor CPs (D–A CPs), do not show a clear glass transition when measured by conventional DSC using simple heat and cool scan. In this work, we discuss the origin of the difficulty for measuring  $T_g$  in such type of polymers. The changes in specific heat capacity ( $\Delta c_p$ ) at  $T_g$  were accurately probed for a series of CPs by DSC. The results showed a significant decrease in  $\Delta c_p$  from flexible polymer ( $0.28 \text{ J g}^{-1} \text{ K}^{-1}$  for polystyrene) to rigid CPs ( $10^{-3} \text{ J g}^{-1} \text{ K}^{-1}$  for a naphthalene diimide-based D–A CP). When a conjugation breaker unit (flexible unit) is added to the D–A CPs,

we observed restoration of the  $\Delta c_p$  at  $T_g$  by a factor of 10, confirming that backbone rigidity reduces the  $\Delta c_p$ . Additionally, an increase in the crystalline fraction of the CPs further reduces  $\Delta c_p$ . We conclude that the difficulties of determining  $T_g$  for CPs using DSC are mainly due to rigid backbone and semicrystalline nature. We also demonstrate that physical aging can be used on DSC to help locate and confirm the glass transition for D–A CPs with weak transition signals. © 2019 Wiley Periodicals, Inc. *J. Polym. Sci., Part B: Polym. Phys.* 2019

**KEYWORDS:** conjugated polymers; glass transition; heat capacity; organic electronics; specific heat capacity

**INTRODUCTION** With unique tunable electronic and optical properties, conjugated polymers (CPs), which are lightweight, flexible and deformable, have drawn significant interest.<sup>1–6</sup> Most of research studies are focused on improving the charge mobility, optical band gap, and processability by engineering chemical structures of CPs.<sup>7–9</sup> However, there is a lack of understanding of their thermo-properties, such as glass transition temperature ( $T_g$ ) for CPs, especially for donor–acceptor polymers (D–A CPs) that possess record breaking device performance.<sup>10,11</sup>  $T_g$  is an important physical parameter that determines the processing condition and end-use temperature of a given polymeric material. When a polymer goes through the glass transition, its modulus can vary by two to three orders of magnitude, dropping from GPa level for glassy state to MPa level for viscoelastic state.<sup>12,13</sup>

For flexible or deformable electronics, it is desired to have a low modulus close to kPa range to match the modulus of human skin; hence, soft CPs with  $T_g$  lower than room temperature are preferred. In addition, the common practice in device fabrication requires an annealing process after depositing a polymer film, to facilitate ordered morphology and improve the charge transport mobility.<sup>1</sup> Such process needs to be carried out at a temperature above  $T_g$  to accelerate molecular dynamics. Additionally, operating devices above its  $T_g$  would cause change in the device morphology and potentially cause performance degradation over time.<sup>14–16</sup> As such, it is important to know the  $T_g$  of the CPs.

Our recent review has briefly summarized several experimental techniques which have been used to measure the  $T_g$  of

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CPs, including differential scanning calorimetry (DSC), AC-chip calorimetry, dynamic mechanical analysis (DMA), and so forth.<sup>17</sup> Among them, AC-chip and DMA are successful in measuring  $T_g$  of D–A CPs,<sup>18,19</sup> whereas DSC, which has been widely used in nonconjugated and flexible polymers, often fails to detect  $T_g$  of D–A CPs even with adequate sample mass.<sup>20,21</sup> ( $T_g$  discussed herein refers to backbone  $T_g$ .) For example, it has been shown that for diketopyrrolopyrrole-based (DPP) polymers, neither conventional DSC nor Flash DSC exhibits a clear  $T_g$ .<sup>22–25</sup>

In the current work, we discuss the potential origin of difficulty for measuring  $T_g$  for D–A CPs by DSC. We studied the specific heat capacities ( $c_p$ ) of several CPs, both conventional and D–A CPs, including poly(3-hexylthiophene) (P3HT) and poly(3-(4'-methylpentyl)thiophene) P3(4MP)T, DPP, and naphthalene diimide-based (NDI) polymers, with standard sapphire reference method<sup>26</sup> using conventional DSC (Mettler Toledo DSC 3+ with FRS 6+ sensor). This measurement follows an ASTM international standard method for determining the specific heat capacity of a given material as a function of temperature. The methodology will be discussed in detail in the following experimental section. The specific heat capacity change between glassy state and liquid state ( $\Delta c_p = c_{p,l} - c_{p,g}$ ,  $l$  and  $g$  refer to liquid state and glassy state) at  $T_g$  for each material is obtained and compared with that for polystyrene (PS), a physical model polymer. The results show that  $\Delta c_p$  of CPs is at least one order of magnitude smaller than that of PS. We hypothesize that there are two reasons for the decrease in  $\Delta c_p$ . First, increased conjugation with large aromatic rings in the polymer backbone resulted in high backbone rigidity yielding a minimal conformation change above and below the  $T_g$ . We tested our hypothesis by designing a flexible alkyl conjugation-break linker (CBL) to restore backbone flexibility, thus enhancing the  $\Delta c_p$ . Second, semicrystalline nature restricts the amount of amorphous phase

presented in the film, thus reducing the  $T_g$  signal which is dependent on amorphous phase content. We used flash scan DSC (Mettler Toledo Flash DSC 2+) to investigate the effect of crystallinity on  $\Delta c_p$ , which dropped substantially with the increased degree of crystallinity. We end this work by providing several potential ways to improve the accuracy of measuring  $T_g$  of D–A CPs.

## EXPERIMENTAL

### Materials

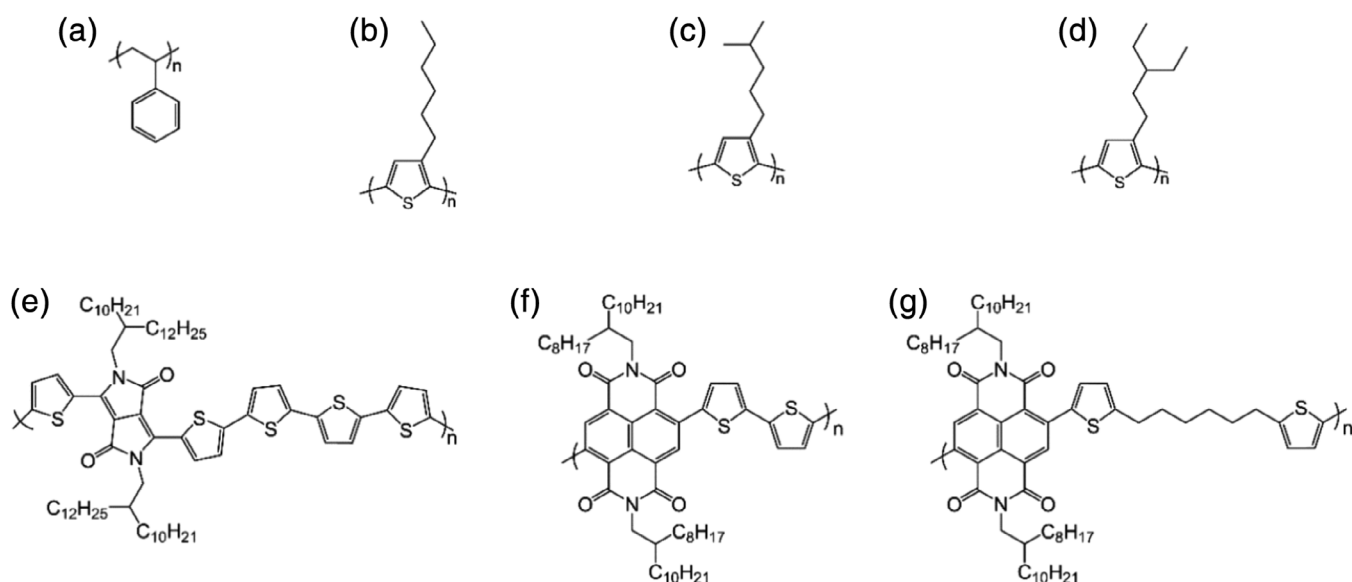
Chemical structures of the materials investigated in the current work are shown in Figure 1.

PS (number-average molecular weight  $M_n$  of 173 kg mol<sup>−1</sup> and PDI of 1.06, Polymer Source, Inc.) and regioregular (r-reg) P3HT (Sigma-Aldrich, regioregularity ~ 92%,  $M_n$  = 24.7 kg mol<sup>−1</sup> and PDI = 2.52) were purchased and used as received.

R-reg P3(4MP)T ( $M_n$  = 20.5 kg mol<sup>−1</sup> and PDI = 1.51) and poly[3-(2'-ethylbutyl)thiophene] P3(2EB)T ( $M_n$  = 14.1 kg mol<sup>−1</sup> and PDI = 1.53) were synthesized by a modified GRIM method as reported in the literature.<sup>27–30</sup> The polymers have very high regularities of over 97%.

Poly[[*N,N'*-bis(2-octyldodecyl)-naphthalene-1,4,5,8-bis-(dicarboximide)-2,6-diyl]-alt-5,5'-(2,2'-bithiophene)] PNDI-C0 ( $M_n$  = 157.5 kg mol<sup>−1</sup> and PDI = 1.99), also known as P(NDI2OD-T2), and poly[[*N,N'*-bis(2-octyldodecyl)-naphthalene-1,4,5,8-bis-(dicarboximide)-2,6-diyl]-alt-5,5'-(E)-2-(2-(thiophene-2-yl)-hexane-1,6-diyl)thiophene)] PNDI-C6 ( $M_n$  = 18.0 kg mol<sup>−1</sup> and PDI = 1.30) were synthesized with a modified approach as illustrated in the Supporting Information.

Poly[diketopyrrolopyrrole-*co*-terthiophene] PDPP-T3 ( $M_n$  = 27.0 kDa and PDI = 3.2) was synthesized as reported in the literature.<sup>31</sup> Molecular weight and PDI were estimated from high-temperature



**FIGURE 1** Chemical structures of the polymers investigated: (a) PS, (b) P3HT, (c) P3(4MP)T, (d) P3(2EB)T, (e) PDPP-T3, (f) PNDI-C0, and (g) PNDI-C6.

gel permeation chromatography (EcoSEC; Tosoh Bioscience) at 200 °C in 1,2,4-trichlorobenzene calibrated by monodisperse PS standards.

## Measurements

### Specific Heat Capacity

The specific heat capacity ( $c_p$ ) measurements of PS, P3HT, P3(4MP)T, PDPP-T3, PNDI-C0, and PNDI-C6 were performed with the Sapphire method by following ASTM E1269-11<sup>26</sup> on Mettler-Toledo DSC 3+. Dry nitrogen purge gas at a flow rate of 20 mL min<sup>-1</sup> was applied during the tests. The instrument was calibrated with indium. The sapphire disc standard (ME51140818) was purchased from Mettler-Toledo. The mass of DSC pans utilized in the measurements were within  $\pm 0.01$  mg to improve the accuracy. The sample mass was between 10 and 20 mg. The measurement for each material composes three separate tests: blank scan, sapphire standard scan, and sample scan, with the same temperature program. A heating/cooling rate of 10 K min<sup>-1</sup> was employed, and the heat-cool-heat temperature range varied with the sample. (The scope of current work focuses on the backbone  $T_g$ . Hence, the DSC temperature profile was not cover the side chain glass transition region, which typically occurs below -40 °C.<sup>17</sup>) The heat flow of second heating scan of sapphire and sample was corrected by subtracting the baseline (blank scan). After correction,  $c_p$  of the sample was calculated by the following equation:

$$c_{p,s} = \frac{\dot{Q}_s \cdot m_{\text{sap}}}{\dot{Q}_{\text{sap}} \cdot m_s} c_{p,\text{sap}} \quad (1)$$

where  $\dot{Q}$  and  $m$  are the corrected heat flow and specimen mass, subscript  $s$  and  $\text{sap}$  stand for sample and sapphire, respectively. The value of  $c_{p,\text{sap}}$  at a given temperature was obtained from the literature report.<sup>32</sup>

### Isothermal Crystallization Measurement

The isothermal crystallization measurements of P3(2EB)T were performed on Mettler-Toledo Flash DSC 2+. The MultiSTAR UFS 1 sensor was conditioned and corrected prior to the measurements. The bulk sample was then cut into small piece with a scalpel under the microscope and then transferred to the active heating area on the MultiSTAR UFS 1 sensor with an animal hair. A premelting step was performed to ensure good thermal contact between sample and sensor membrane. A high heating/cooling rate of 1000 K s<sup>-1</sup> was employed to ensure the material reaches the disordered supercooled state during cooling and increase the signal to noise ratio. The measurements were carried out by the following temperature program: first, sample was heated to 250 °C, which is above the melting temperature, and held for 10 ms; then, the sample was cooled down to the crystallization temperature of 90 °C, and held there for different times to allow the sample to crystallize; after that, the sample was cooled down to -20 °C and then reheated to 250 °C. The data analysis was performed on the reheating scan.

### Modified DMA

Modified DMA measurements were performed on PNDI-C0 by solution casting the sample on glass fiber. The coated glass fiber was then measured on a TA Instruments Q800 DMA (New Castle, Delaware) under strain-controlled mode. A temperature ramp with heating rate of 3 K min<sup>-1</sup> and frequency of 1 Hz was conducted. The strain was in the linear regime.

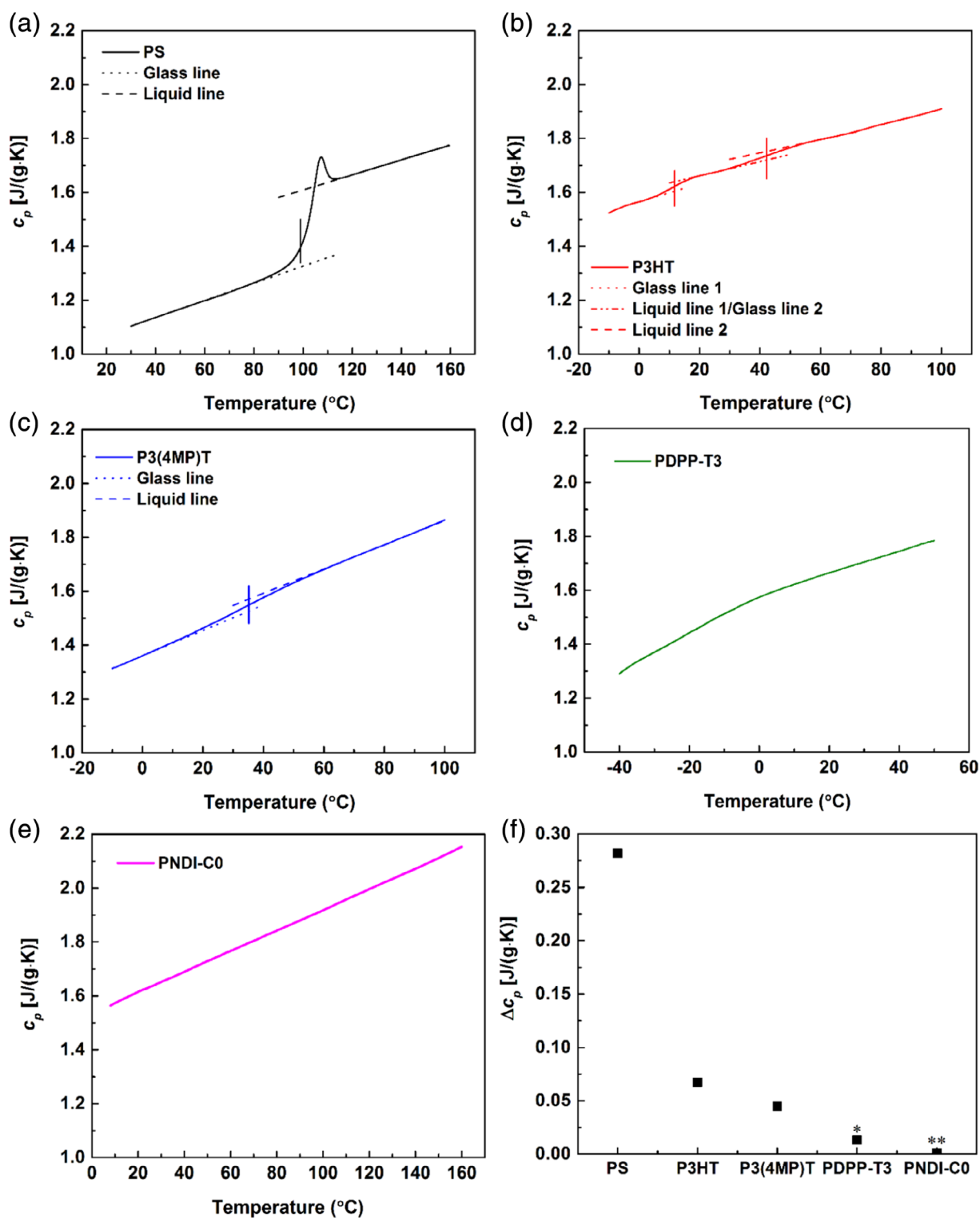
### Solution X-ray Scattering

Solution X-ray scattering was performed at Stanford Synchrotron Radiation Lightsources under beam line 4-2 at 15 keV. Samples were prepared at 5 mg mL<sup>-1</sup> in chlorobenzene at ambient conditions and allowed to dissolve overnight. Capillary-based flow cells were utilized to mitigate the effect of capillary thickness and curvature on background scattering for accurate subtraction of solvent and capillary. Neat anhydrous chlorobenzene solvent was measured prior to each CP solution for background subtraction. Each scattering experiment was performed at room temperature and run for 5 min for an adequate signal to noise ratio. And subsequently analyzed using SasView fitting software (<http://www.sasview.org/>).

## RESULTS AND DISCUSSION

First, we discuss the methodology we used to accurately determine the  $\Delta c_p$ . Sapphire method determines the  $c_p$  of a sample by calibrating the sample heat flow signal with the signal of sapphire standard which has known  $c_p$  (shown in Fig. S1).<sup>26</sup> For the  $c_p$  curve of a sample, when a step change in  $c_p$  can be readily observed, the temperature range of glassy state and liquid state was then determined and fitted with two different straight lines, respectively. Then, we calculate  $T_g$  and  $\Delta c_p$ . For example, in the case of PS, the glassy range and liquid range can be readily determined with an obvious step change, as shown in Figure 2(a). We first obtained the  $\Delta c_p$  of PS and compared to the literature value. Then,  $T_g$  was calculated based on the half-step method<sup>33</sup> or Moynihan method<sup>34</sup> depending on each specific case. In the case where glass transition region cannot be readily defined, a second technique, such as DMA, was conducted to get a rough estimate of  $T_g$ . After that, based on one of the signatures of glass, enthalpy overshoot,<sup>35</sup> which happens when heating up an aged glass or in the case where the cooling rate/heating rate ratio less than 1, a physical aging experiment [temperature program schematically shown in Fig. S2(a)] or cooling rate experiment was performed on DSC to confirm the glass transition region, and  $\Delta c_p$  was then determined. More detailed discussions are presented subsequently.

We performed the measurements on four CPs [P3HT, P3(4MP)T, PDPP-T3, PNDI-C0] and plotted  $c_p$  as a function of temperature in Figure 2. Due to the scope of the current work, we limit our discussion herein on the temperature range at the vicinity of the glass transition. DSC heating scans in the full temperature range are provided in Fig. S3, Supporting Information. All CPs are semicrystalline since they all show a melting peak upon heating to high temperature. As expected,



**FIGURE 2** Specific heat capacities (solid line) of (a) PS, (b) P3HT, (c) P3(4MP)T, (d) PDPP-T3, and (e) PNDI-C0 obtained from the Sapphire method using a conventional DSC with  $10\text{ K min}^{-1}$  heating/cooling rate (Second heating scans were used for data analysis.). The dotted line and dash lines are the glass line and liquid line, respectively, to determine  $T_g$  and heat capacity change  $\Delta c_p$  at  $T_g$ . The vertical lines in (a–c) mark the position of  $T_g$ . (f) The heat capacity change  $\Delta c_p$  at  $T_g$  for PS, P3HT, and P3(4MP)T.  $\Delta c_p$  of P3HT is the total change of the two-step transition. \*Data estimated from apparent  $c_p$  curve in Figure S3(b). \*\*Estimated value based on the curvature difference in part (d) and (e). [Color figure can be viewed at [wileyonlinelibrary.com](http://wileyonlinelibrary.com)]

the glass transition of PS can be readily observed together with a typical enthalpy relaxation peak in Figure 1(a). The  $T_g$  of PS determined by Moynihan method<sup>34</sup> is 99.0 °C. We obtained  $\Delta c_p$  at  $T_g$  by calculating the difference between the extrapolated liquid line and glass line, which gives a value of 0.28 J g<sup>-1</sup> K<sup>-1</sup> and has a good agreement with the literature report value of 0.28–0.30 J g<sup>-1</sup> K<sup>-1</sup>.<sup>36,37</sup>

Turning to the CPs, we observed a much weaker glass transition both for P3HT and P3(4MP)T, as shown in Figure 2(b,c), respectively. For P3HT, it features a two-step transition where the first step with a  $T_g$  of 11.7 °C (this value shows great agreement the literature reported value of 12–14 °C measured with DSC and DMA.<sup>15,38–41</sup>) is associated with the mobile amorphous fraction and the second one with a  $T_g$  of 42.2 °C is related to the rigid amorphous fraction. This is consistent with previous work by Remy et al.<sup>42</sup> Upon tuning the side chain isomerism, surprisingly, P3(4MP)T only gives a one-step transition with a  $T_g$  of 35.2 °C. Such a difference is presumably related to the difference in crystalline morphology and requires further investigation in future. The comparison of  $\Delta c_p$  at  $T_g$  among PS, P3HT, and P3(4MP)T is depicted in Figure 2(f), in which we see a much smaller  $\Delta c_p$  for P3HT isomers [0.067 J g<sup>-1</sup> K<sup>-1</sup> for P3HT and 0.045 J g<sup>-1</sup> K<sup>-1</sup> for P3(4MP)T]. Such a small  $\Delta c_p$  for r-reg P3HT and P3(4MP)T herein is presumably related to rigid backbone, and semicrystalline nature. We will discuss the effects of backbone rigidity (in terms of persistence length) and crystallinity [in terms of relative degree of crystallinity (RDOC)] on  $\Delta c_p$  in more detail in the following section.

DSC measurements for PDPP-T3 and PNDI-C0, which have highly planar and rigid backbone structures, are presented in Figure 2(d,e), the step change in  $c_p$ , thus the glass transition, cannot be readily seen from the DSC scans. A linear curve is observed and is expected based on various previous reports.<sup>21–24,43–47</sup> PDPP-T3 shows a small curvature at the vicinity of 0 °C. Zhang et al. recently reported a  $T_g$  of ~20 °C both from AC-chip calorimetry and modified DMA.<sup>19</sup> In general, the  $T_g$  obtained from AC-chip and DMA is 10–20 °C higher than that from conventional DSC.<sup>18</sup> Hence, the slight change in slope near 0 °C in Figure 2(d) is related to the glass transition of the PDPP-T3 backbone. We further conformed this by performing the physical aging experiments [see temperature profile Fig. S2 (b)], where sample was purposely aged at 0, –5, and –10 °C, respectively, for 60 min before reheating up. The resultant DSC heating scans are plotted in Figure S4(a) and enthalpy overshoots resulted from structure recovery were observed in all three aging temperatures. We then estimated its  $\Delta c_p$  from the baseline subtracted apparent  $c_p$  curve, which is approximately 0.013 J g<sup>-1</sup> K<sup>-1</sup> with a  $T_g$  of ~2.2 °C, as presented in Figure S4 (b). For PNDI-C0, we could not determine the exact value of  $\Delta c_p$ . The value is expected to be lower than PDPP-T3, on the order of 10<sup>-3</sup> J g<sup>-1</sup> K<sup>-1</sup> or smaller, owing to the almost linearly increased  $c_p$  over the temperature range we investigated.

### Effect of Backbone Rigidity

Based on our experimental findings, we hypothesize that the increase in backbone rigidity causes a drop in the  $\Delta c_p$ . For

example, it has been reported for poly(*n*-alkyl methacrylate)s, with the increase of *n*-alkyl side chain length, the persistence length ( $l_p$ ) increases, that is, backbone becomes more rigid.<sup>48,49</sup> Meanwhile, a decrease in  $\Delta c_p$  is observed as side chain length increases.<sup>50</sup> In the case of P3HT, r-reg P3HT has a more rigid backbone ( $l_p$  of 2.9 nm) compared with regiorandom (r-ran) P3HT ( $l_p$  of 0.9 nm)<sup>15,51</sup> and PS ( $l_p$  of 0.7 nm),<sup>52,53</sup> as shown above, a significant decrease in  $\Delta c_p$  is observed. (It has been reported that r-ran P3HT, which is amorphous and more flexible, gives a  $\Delta c_p$  of approximately 0.3 J g<sup>-1</sup> K<sup>-1</sup>,<sup>42,54</sup> which is close to the value of PS.) Same argument is applicable to P3(4MP)T, which has a  $l_p$  of approximately 2–2.5 nm,<sup>55</sup> similar to that of r-reg P3HT. While for DPP-based D-A CPs, they tend to have even large  $l_p$  than r-reg P3HT due to more rigid backbone.<sup>56</sup> Hence, we see a much smaller  $\Delta c_p$  for PDPP-T3.

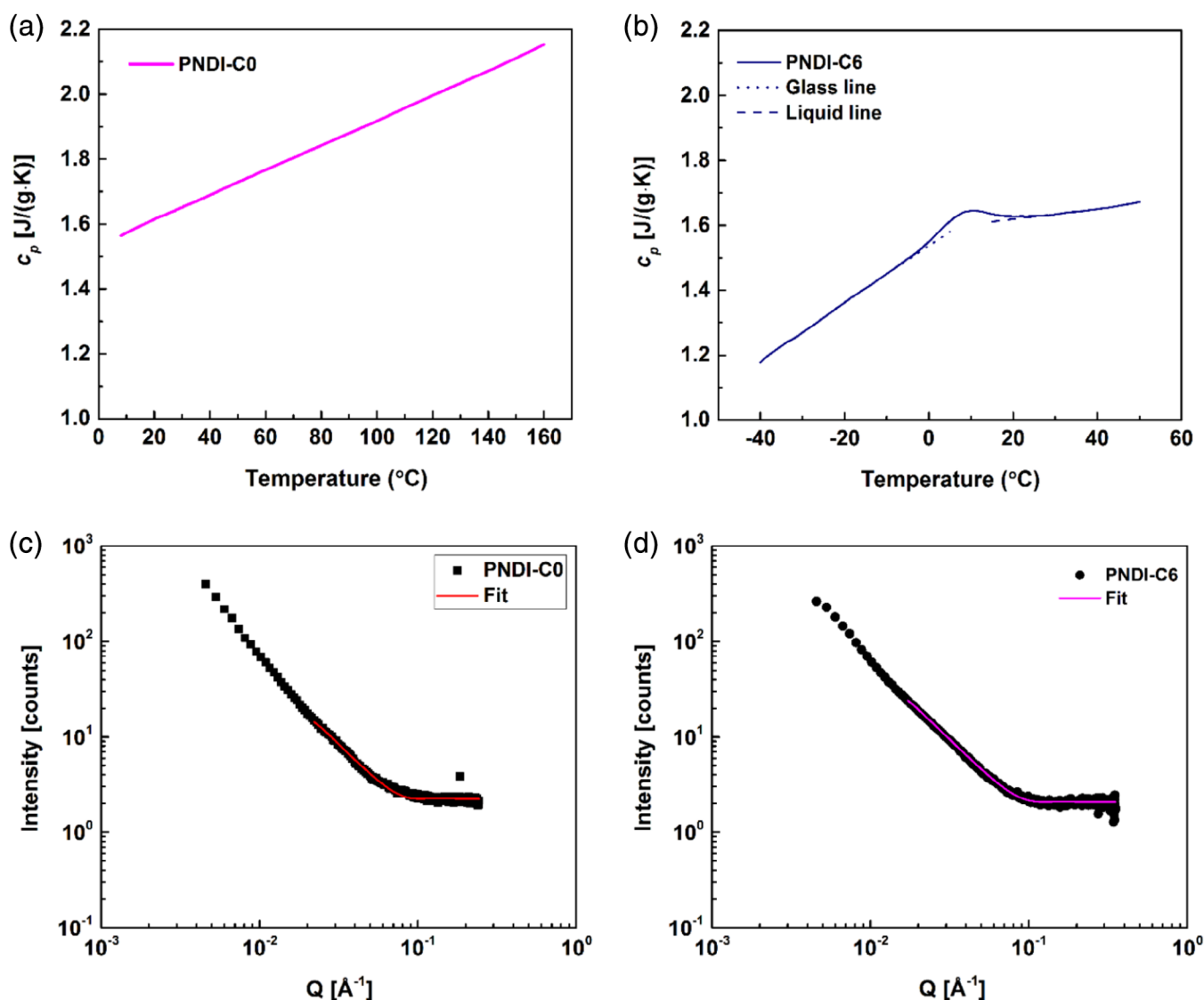
Such hypothesis was tested by engineering D-A CPs with different backbone rigidities by introducing flexible alkyl CBL into the D-A CPs [chemical structure shown in Fig. 1(g)] and measuring  $\Delta c_p$ . We measured both PNDI-C0 (fully conjugated) and PNDI-C6 (with nonconjugated flexible segment) and studied the effect of the conjugation breaker on  $T_g$  (Fig. 3) as well as the backbone rigidity (Fig. S7). The glass transition region became more obvious [Fig. 3(b)] when a 6-carbon CBL was incorporated to the backbone repeating unit of PNDI-C0 [Fig. 3(a)]. The  $T_g$  of PNDI-C6 was determined to be –0.1 °C with a  $\Delta c_p$  of 0.052 J g<sup>-1</sup> K<sup>-1</sup>, which is in the same range as P3HT and P3(4MP)T, and at least one order of magnitude greater than the  $\Delta c_p$  of fully conjugated PNDI-C0. The glass transition region of PNDI-C6 was confirmed with the physical aging and cooling rate dependence experiments. In both cases, enthalpy overshoot is observed on heating scans, as shown in Figure S5.

The reduction in backbone rigidity with the presence of CBL was verified through solution small angle X-ray scattering (SAXS) for polymers dissolved in chlorobenzene. Modeling of the scattering data enabled approximate persistent lengths to be determined. In our case, the polymer aggregation presented at the room temperature prohibits reliable quantitative data fitting in the low scattering vector region near the beam stop. We used the flexible cylinder model, a model that generally used to fit semirigid polymer, to fit the solution scattering data, as shown in Figure 3(c,d).<sup>57</sup> The raw data of solution scattering are shown in Figure S6. The fitting parameters are listed in Table S1. With the flexible cylinder model, we estimate a 40% reduction in  $l_p$  upon introducing flexible alkyl chain to PNDI-C0. Future investigations at lower concentration and elevated temperatures are warranted to mitigate aggregation and elucidate the Guinier regime for precise quantitative analysis.

### Effect of Crystallinity

It has long been recognized that for conventional semicrystalline polymers, the glass transition phenomenon depends on the degree of crystallinity, including the width of glass transition region,  $T_g$  and  $\Delta c_p$ . However, there is little work performed on understanding the effect of RDOC on the  $T_g$  of CPs

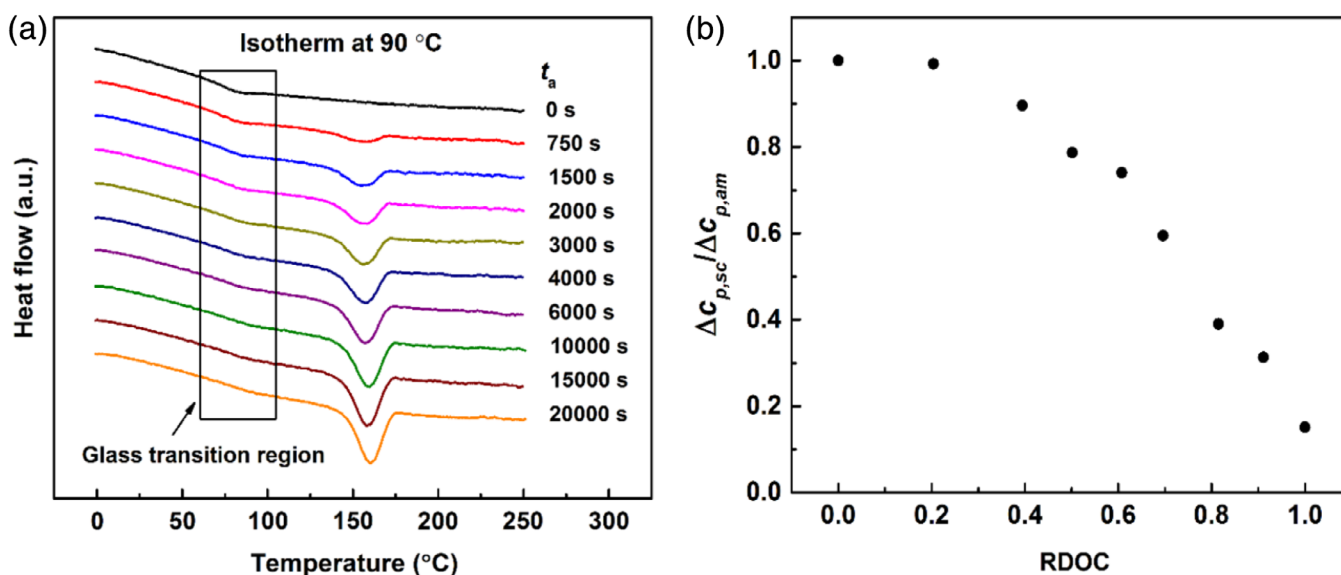




**FIGURE 3** Restoration of  $\Delta c_p$  by reducing the backbone rigidity. The specific heat capacities (solid line) of (a) PNDI-C0 and (b) PNDI-C6 obtained from the Sapphire method with conventional DSC. The dotted line and dashed lines in (b) are glass line and liquid line, respectively. (In addition, we notice that surprisingly the glassy lines of PNDI-C0 and PNDI-C6 do not have same slope, which we do not know the exact origin at this point.) (c,d) The solution X-ray scattering results and the flexible cylinder model fit for PNDI-C0 and PNDI-C6. [Color figure can be viewed at [wileyonlinelibrary.com](http://wileyonlinelibrary.com)]

due to experimental challenges associated with trapping samples into desired RDOC. Experimentally, precisely controlling the RDOC for CP is not straightforward. In general, the conventional DSC is not capable to quench the CPs to the supercooled, or completely amorphous state owing to the fast crystallization rate of CPs.<sup>15,20,25,38,58–61</sup> For example, as shown in Figure S7, the crystallization of P3(2EB)T is inevitable upon cooling it from its melt state with conventional DSC even at  $100 \text{ K min}^{-1}$ , while faster cooling speed using flash DSC can trap P3(2EB)T into the fully amorphous phase using a cooling rate of  $60,000 \text{ K min}^{-1}$  ( $1,000 \text{ K s}^{-1}$ ), as shown in Figure 4 subsequently. This trapped amorphous glass can be heated up to its crystallization temperature and vary the isothermal crystallization time to precisely control the degree of crystallinity.

In this work, we demonstrated P3(2EB)T with different RDOCs by varying the isothermal crystallization time at  $90^\circ\text{C}$  after quenching it from the melt state. The temperature profile is schematically presented in Figure S8.<sup>62</sup> The corresponding reheating scans are presented in Figure 4(a), in which the area of the melting peak grows with the crystallization time and in the meantime, the glass transition region broadens. We integrated the melting peak area near  $160^\circ\text{C}$  (shown in Fig. S9) and compared the RDOC ( $\text{RDOC} = A_t/A_{20,000}$ ,  $A_t$  is the peak area at crystallization time  $t$ ). And the resultant normalized  $\Delta c_p$  is depicted in Figure 4 (b) as a function of RDOC. As expected, a decrease in normalized  $\Delta c_p$  is observed with the increase of RDOC. When RDOC is above 0.2, the normalized  $\Delta c_p$  almost linearly decreases with RDOC (more crystalline domain, less entropy change during the glass



**FIGURE 4** Controlled isotherm crystallization of CPs and its effect on glass transition. (a) Reheating scans of P3(2EB)T after isothermal crystallization at 90 °C for different times (as indicated in the legend) measured with flash DSC. (b) Apparent  $\Delta C_{p,sc}$  at  $T_g$  for P3(2EB)T at different RDOC normalized by the apparent  $\Delta C_{p,am}$  at fully amorphous state. [Color figure can be viewed at [wileyonlinelibrary.com](http://wileyonlinelibrary.com)]

transition). The relative change in  $\Delta C_p$  clearly shows a significant decrease for P3(2EB)T at high RDOC, which then explains the difficulty in obtaining  $T_g$  from conventional DSC for semicrystalline CPs. Meantime, an elevation in  $T_g$  is observed as shown in Figure S10.

In addition, since P3(2EB)T is able to be quenched into fully amorphous state with Flash DSC, the effects of chain rigidity and crystallization can be deconvoluted. Based on the symmetric line analysis method,<sup>63–67</sup> we estimated the sample mass of P3(2EB)T in Flash DSC measurement to be approximately 67 ng. Hence, the  $\Delta C_{p,am}$  at  $T_g$  for the fully amorphous P3(2EB)T is calculated to be approximately  $0.14 \text{ J g}^{-1} \text{ K}^{-1}$ , two times smaller than PS and r-ran P3HT ( $0.28\text{--}0.3 \text{ J g}^{-1} \text{ K}^{-1}$ ). (The procedures of the calculations are described in detail in Supporting Information and Fig. S11.) In addition, the second heating curve of r-reg P3HT [Fig. S3(b)] gives an enthalpy of fusion ( $\Delta H_m$ ) of  $16 \text{ J g}^{-1}$ , given that the enthalpy of fusion of perfect P3HT crystal ( $\Delta H_m^\infty$ ) in the literature spans from 33 to  $99 \text{ J g}^{-1}$ ,<sup>68–76</sup> we estimate that the absolute crystallinity ( $X_c = \Delta H_m / \Delta H_m^\infty$ ) of r-reg P3HT here should range from 16 to 49% depending on the value of  $\Delta H_m^\infty$ . Hence, the  $\Delta C_{p,am}$  at  $T_g$  for the fully amorphous r-reg P3HT is estimated between 0.08 and  $0.13 \text{ J g}^{-1} \text{ K}^{-1}$ , which is in a similar range to that of r-reg P3(2EB)T. Besides, as r-reg P3(2EB)T, P3(4MP)T, and P3HT are isomers,  $l_p$  is presumably 2–3 nm. Recall that PS and r-ran P3HT possess a  $l_p$  of 0.7 and 0.9 nm, respectively, demonstrating higher flexibility than r-reg P3(2EB)T and r-reg P3HT, which corresponds well with the higher  $\Delta C_p$  of PS and r-ran P3HT. (We also performed the Flash DSC measurement on PDPP-T3 and PNDI-C0 with UFH 1 sensor. However, as shown in Fig. S12, the crystallization during cooling is inevitable even with cooling rate up to  $10,000 \text{ K s}^{-1}$ .) Recently, Yin et al. investigated the glass transition behavior for polymers of intrinsic microporosity, which are nonconjugated but also possess rigid

backbone, low  $\Delta C_p$  of  $0.16 \text{ J g}^{-1} \text{ K}^{-1}$  has been observed.<sup>77</sup> Therefore, this indicates a correlation between small  $\Delta C_p$  and rigid chain, or large  $\Delta C_p$  for flexible chain.

Based on the results present above, we see that D–A CPs in general possess a low  $\Delta C_p$  at  $T_g$  (more than one order of magnitude smaller than PS), which limits the application of conventional DSC in measuring  $T_g$ . This is presumably owing to the following three factors: rigid backbone, semicrystalline nature, and high side chain content.

1. In order to improve the electrical performance, D–A CPs are designed in a way which have highly planar and rigid backbone to facilitate high charge transport mobility. Typically, high backbone rigidity reduces the entropy of the chain conformation near the glass transition.
2. Many D–A CPs are semicrystalline. In general, the crystallization rate of D–A CPs is high compared with the cooling rate of a conventional DSC, that is, it is difficult to melt D–A CPs and quench them into a fully amorphous state. Since only amorphous fraction contributes to  $T_g$ ,  $\Delta C_p$  is then further reduced. Hence, the overall contributions lead to a low  $\Delta C_p$ .
3. High mass fraction of long and branched flexible side chains is commonly used in the CPS to improve the solubility issue. Meanwhile, it has been suggested for non-CPs, introducing bulky side chains lead to high glassy-state entropy and glassy-state  $c_p$ , while the liquid  $c_p$  is not affected, which then results in a low  $\Delta C_p$  at  $T_g$ .<sup>36,78</sup> Same argument is presumably applicable to D–A CPs.

#### Remedy of Measuring $T_g$ for D–A CPs with Extremely Low $\Delta C_p$

The data presented in Figures 1 and 2 suggest that for a D–A CP with  $\Delta C_p$  lower than  $0.01 \text{ J g}^{-1} \text{ K}^{-1}$ , DSC cannot readily measure its  $T_g$  even with adequate sample mass (e.g., tens of

milligrams). In this scenario, a secondary measurement is recommended to compliment the DSC measurement to locate  $T_g$ . AC-chip and DMA are also widely used to obtain  $T_g$  by measuring the material dynamics, which do not rely on the magnitude of  $\Delta c_p$ . Though AC-chip has a higher sensitivity, it is not readily available for most research groups. In the case of modified DMA, it cannot obtain the absolute moduli due to unspecified sample geometry when supported by another substrate and this might cause difficulty in distinguishing glass transition phenomenon with various other phase transitions (e.g., melting, liquid crystalline transition) in CPs.<sup>79</sup> In addition, since several thermal transitions exhibit a peak in  $\tan \delta$  response, which potentially introduces challenges to accurately measure  $T_g$ . Therefore, we suggest combining the modified DMA herein with DSC to help unravel the missing  $T_g$ .

This methodology is rather simple. One first roughly estimate the potential temperature range for glass transition from DMA, followed by a physical aging measurement or cooling rate dependence measurement on DSC to confirm the  $T_g$  of CPs. The design of such methodology is based on one signature of glass, that is, enthalpy overshoot,<sup>35</sup> which is a phenomenon long been recognized for glass. When a material is cooled from equilibrium state, the mobility decreases until it is not long able to maintain the equilibrium at given experimental timescale. As a result, glass transition takes place, and material goes to the glassy state, which is in the nonequilibrium state. The resultant enthalpy change is schematically shown in Figure S13. Due to the excess enthalpy in the glassy state compared with equilibrium state, the material has a tendency to relax toward the equilibrium. This process is known as physical aging or structure recovery. In this case, when an aged sample is reheated up, the response evolves parallelly to the glassy line. As it crosses the equilibrium line, due to the lower mobility compared with unaged sample, the response cannot follow the heating rate and leads to an overshoot in enthalpy. As the temperature being further increased, the material is finally mobile enough to follow the heating rate and reach to the equilibrium state.<sup>35</sup> Similarly, when a slow cooled sample is fast heated, since it relaxes more during cooling, an enthalpy overshoot also appears on the heating curve. Figures S14(a) and S14(b) plot the heat flow curves of PS obtained from physical aging experiments<sup>80</sup> and cooling rate dependence experiments.<sup>81</sup> It is readily seen that apart from the glass transition region, in which the enthalpy overshoot occurs, the glass lines and liquid lines for the aged run and unaged run well overlap on top of each other. This is also true for the heating scans in the cooling rate experiments. Hence, we can use these two experiments to improve the accuracy of locating the glass transition region, glass line and liquid line. (We remark here that there are different methods, half-step,<sup>33</sup> Moynihan method, and<sup>34</sup> inflection point,<sup>82</sup> to obtain  $T_g$  value from DSC scans. Regardless, cooling rate dependence and aging experiments are highly recommended for verifying the validity of  $T_g$ , especially for material with extremely low  $\Delta c_p$ .)

Here, we use PNDI-C0 as an example to illustrates what can be done to probe the CPs with weak  $T_g$ . Although a direct

heating scan on DSC does not show any sign of  $T_g$  [Fig. 1(e)], careful experimental design based on the signature of glass transition, which is enthalpy relaxation, can be utilized to reveal the glass transition region on DSC. We have demonstrated the enthalpy relaxation in Figures S3 and S5 for PDPP-T3 and PNDI-C6, both have  $\Delta c_p$  larger than NDI-C0, which is easy to measure. This physical aging experiment could also work on PNDI-C0, and we performed the aging experiment for PNDI-C0 at 70 °C. We first roughly estimated the  $T_g$  for PNDI-C0 using DMA results of PNDI-C0 thin film as shown in Figure S15(a). A peak in  $\tan \delta$  appears at 137.21 °C, which is presumably the  $T_g$  associated with the backbone motion of the PNDI-C0. Figure S15 (b) plots the comparison of DSC scans between unaged and aged conditions, in which an enthalpy overshoot is observed in the temperature range of approximately 80–120 °C. We estimated the  $T_g$  from the unaged condition, which gives approximately 101.9 °C with apparent  $\Delta c_p$  of approximately  $2.4 \times 10^{-3} \text{ J g}^{-1} \text{ K}^{-1}$ .

## CONCLUSIONS

In summary, the glass transition of a series of CPs, including conventional thiophene-based CPs [P3HT and P3(4MP)T] and D-A CPs (PDPP-T3, PNDI-C0, and PNDI-C6), was investigated with DSC. ASTM E1269-11 method using sapphire as a reference sample was employed to measure  $c_p$ . In addition, flash DSC measurements were conducted on P3(2EB)T to establish the effect of crystallinity on  $\Delta c_p$ , where  $\Delta c_p$  exhibits significant decrease as crystallinity increases. The results show that CPs possess a much lower  $\Delta c_p$  compared with PS ( $0.28 \text{ J g}^{-1} \text{ K}^{-1}$ ), especially for D-A CPs, which can be as low as in the order of  $10^{-3} \text{ J g}^{-1} \text{ K}^{-1}$ . Such low  $\Delta c_p$  is mainly owing to the rigid backbone and high side chain content as well as semicrystalline nature, which explains the missing  $T_g$  often observed in DSC curves. We also proposed to combine the modified DMA experiments with the physical aging experiments on DSC to improve the accuracy of measuring  $T_g$ , which is found to be successful even for the D-A CPs with  $\Delta c_p$  of  $10^{-3} \text{ J g}^{-1} \text{ K}^{-1}$ .

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